

# ToppersNotes

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**IES/GATE**  
**CIVIL ENGINEERING**

**R C C**

**VOLUME-IV**



# Contents

R C C

1-307



2 RCC - Reinforced Cement Concrete

INTRODUCTION

RCC

① Cement Concrete

- Cement
- sand (fine aggregate)
- stone aggregate (coarse agg)
- water (strength, workability)
- Admixtures (↑ setting rate, plasticisers etc.)

② Reinforcement steel

# I.S. code

① I.S. 456 - 2000

② IS 875 - Loading IS code

③ IS 1893 - Earthquake

④ IS ~~18~~ 13920 - Earthquake detailing

# (A) Cement concrete :-

# (1) Mix

There are two types :-

① Nominal mix :- fixed proportions based on volumetric ratio (for lower mix only - m-15 & m-20) are called NOMINAL MIX.

for e.g. 1 : 2 : 4 → M15

1 : 1½ : 3 → M20

\* The properties of different materials used are not considered.

\* It is assumed that required strength will be obtained.

① Design Mix:- (For M-25 and higher grade only design mix should be used).

The proportion of materials to be mixed to get a particular strength of concrete, based on the quality of actual sample of materials to be used are designed.

\* Actual sample of materials are used and mixed in design proportion. concrete is casted in cubes and tested at 28 days. Only that proportion is suggested that provide the the proportion of required strength is suggested.

② Types of Grades of concrete:-

As per IS-Code:

① Ordinary Concrete

M20 to M25

② Standard Concrete

M25 to M55

③ HIGH STRENGTH CONCRETE

M60 to M80

\* ③ For RCC, Min<sup>m</sup> grade of concrete = M20  
max M40

\* For PSC  
Min<sup>m</sup> grade of Prestension = M40.  
Post tensioned = M30

\* Minimum grade of concrete at different exposure condition:

Table 16

- ① Mild → M20
- ② Moderate → M25
- ③ Severe → M30
- ④ Very severe → M35
- ⑤ Extreme → M40

④ Table 16

Exposure condition:  
 (min<sup>nominal</sup> concrete cover)

- ① Mild → Protected from weather  
 (M20) → Not exposed to Rain
- ② Moderate → ① sheltered from severe rain  
 (M25) ② exposed to rain  
 ③ concrete continuously under water
- ③ Severe (M30) ① exposed to severe rain  
 ② concrete subjected to alternate wetting and drying  
 ③ completely immersed in sea water
- ④ Very severe (M35) ① exposed to sea water  
 (alternate wetting/drying)  
 ② severe freezing  
 ③ subjected to sub soil cond<sup>n</sup> (foundation)

Table 16

Min<sup>m</sup> Nominal cover

20mm

30mm

45mm

50mm

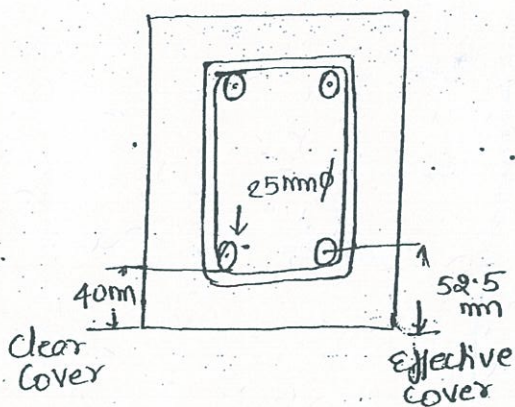
- ⑤ Extreme (M40) ① Member in tidal zone | 75mm  
 ② Member subjected to chemical

#5 NOMINAL COVER:

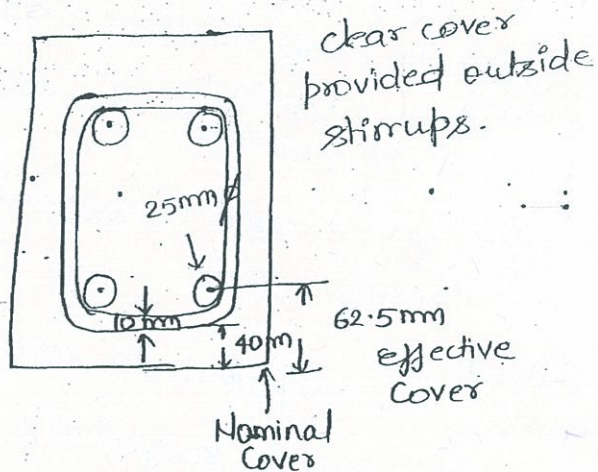
Pr. 26.4 / P-46

→ NOMINAL COVER is the design depth of concrete cover. (clear cover), provided to all types of steel reinforcement, including links:

Nominal cover is the min<sup>m</sup> cover clear cover provided to outermost steel reinforcement. (Main reinforcement or lateral ties, stirrups etc.)



Column (Before 2000)



Column (After 2000)

#	Min <sup>m</sup> Nominal cover (for different type)	Mild Exposure	Severe	extreme
①	slab	20mm	45mm	75mm
②	Beams	25mm	45mm	75mm
③	Columns	40mm	45mm	75mm
④	Found <sup>n</sup>	50mm	50mm	75mm



#1) Nominal cover have been suggested in IS code to avoid corrosion of reinforcement.

#6) Characteristic strength of concrete :-

M 30  
 ↓  
 Mix characteristic strength  $f_{ck} = 30 \text{ N/mm}^2$

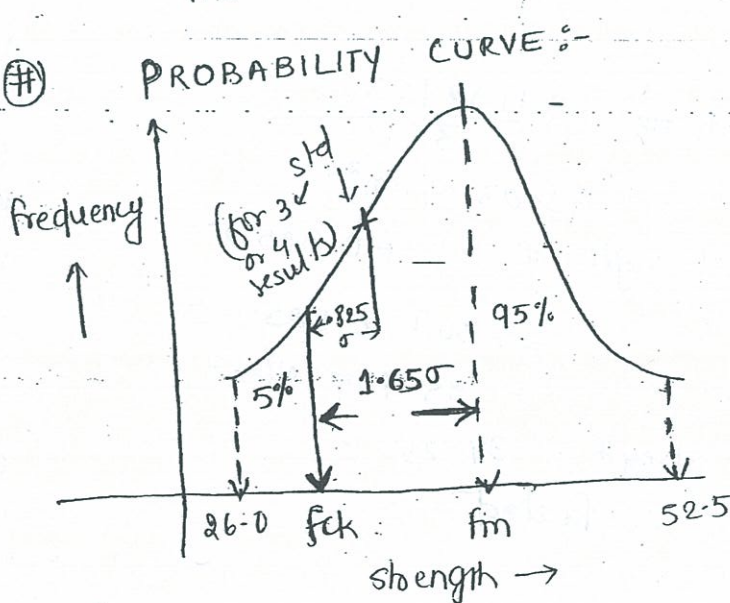
# - Characteristic strength is the value of strength of concrete below which not more than 5% of test results are expected to fall.

\* If 100 test results are taken for a particular concrete.

26.0, 27.5, 28.2, 29.4, 29.7, 30.6, 30.9, 31.2, 31.5,  
 32.0, 32.1 ..... 52.5 (100 test results)

30 is such value of strength below which - 5% results above which - 95% results  
 The above concrete is M30.

#) PROBABILITY CURVE :-



It is a curve plotted for frequency of best results of different values.

$f_{ck}$  → characteristic strength ( $5\% < f_{ck} < 95\%$ )

$f_m$  → Mean strength ( $50\% < f_m < 50\%$ )

•  $f_m = f_{ck} + 1.65\sigma$  → (A) Relation

$\sigma$  → std. deviation.   
  $\sigma$  → no. of test results.

As per IS code

Grade	M10/M15	M20/M25	M30 & Above
$\sigma$	3.5 N/mm <sup>2</sup>	4.0 N/mm <sup>2</sup>	5.0 N/mm <sup>2</sup>

for e.g.

M30 concrete

Mean strength

$$f_m = f_{ck} + 1.65\sigma$$

$$= 30 + 1.65 \times 5.0$$

$$f_m = 38.25 \text{ N/mm}^2$$

Ques.

For M30

Strength obtained

- ① 34.0 N/mm<sup>2</sup>
- ② 32.0 N/mm<sup>2</sup>
- ③ 33.1 N/mm<sup>2</sup>

failed

$f_m$  → design → use

$$\text{avg strength} = \frac{34 + 32 + 33.1}{3}$$

$$= 33.03 \text{ N/mm}^2$$

As per IS code, avg strength  $\neq f_{ck} + 0.825\sigma$

$$= 30 + 0.825 \times 5$$

$$= 34.125 \text{ N/mm}^2$$

∴ avg strength < 34.125

∴ failed

\* Type

I) Initial Tangent Modulus of Elasticity

→ slope of stress strain curve at origin is called initial tangent modulus of elasticity.

This value  $E_{IT} = 5000\sqrt{f_{ck}}$  → Value of  $E_c$  considered by IS code is this value.

II) Tangent Modulus of Elasticity :-

The slope of tangent at any point of curve is called tangent modulus of elasticity.

It is an instantaneous value.

$$E_T = \frac{dy}{dx} = \frac{\text{Stress}}{\text{Strain}}$$

III) Secant Modulus of Elasticity :-

Slope of the line joining any point of curve with origin is called secant modulus.

$$E_s = \frac{\text{Total stress}}{\text{Total strain}} \quad (\text{measured from origin})$$

Ⓐ secant modulus is also called static modulus of elasticity.

(Behaviour under sustained static loading for a long time).

\*  $E_{IT}$  (Initial Tangent) is called Dynamic modulus of elasticity.

(Behaviour of concrete stress/strain in case of impact loading)

\* Within elastic portion of curve :-

$$E_T = E_s = E_{IT} = 5000 \sqrt{f_{ck}}$$

for m30  
Permissible stress  
=  $0.67 \sqrt{f_{ck}}$

\* Value considered is  ~~$E_{IT}$~~ , for design purpose we should consider  $E_c$  value at  $\frac{1}{3}$  of failure stress value)

say  $\sigma_{bc}$  value =  $\frac{1}{3} f_{ck}$ .

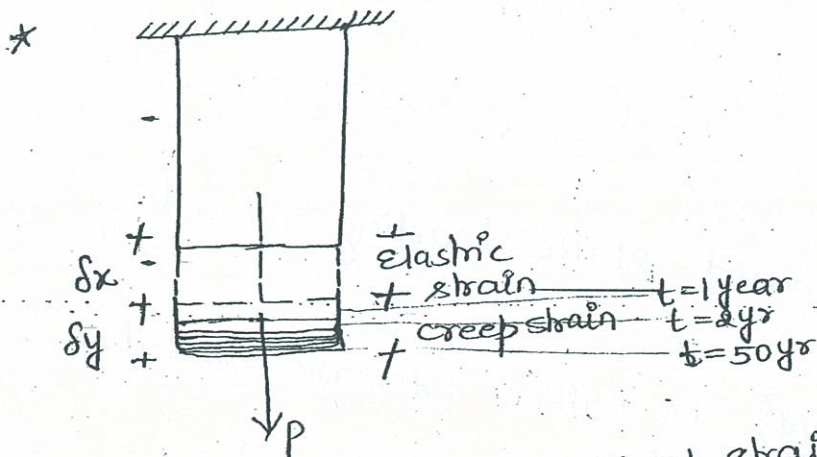
The value considered shall be static modulus of elasticity.

The value will be  $E_c = 5000 \sqrt{f_{ck}}$

(#10) Effect of creep from Young's Modulus of Elasticity:-

# Creep :-

Time dependent deformation under a constant loading, kept for a very long time.



\* creep coefficient =  $\frac{\text{Creep strain (ult.)}}{\text{creep stress}}$

\* For concrete

\* long term modulus of elasticity

Table No. 11

#7 Acceptance Criteria for concrete  
(for day to day quality control at site)

As per 16.1 / Table 1.1

① Mean of the group of 4 (four) Non overlapping consecutive test result

whichever is more  $\left\{ \begin{array}{l} \geq f_{ck} + 0.825\sigma \\ \text{or} \\ \geq f_{ck} + 4 \text{ N/mm}^2 \end{array} \right.$  (rounded off to nearest 0.5 N/mm<sup>2</sup>)

② Individual test result of any sample (ITR Value)  $\geq (f_{ck} - 3) \text{ N/mm}^2$

③ As per 15.4 The test result of sample shall be average of three specimens.

The individual variation  $\neq \pm 15\%$  of average value.

Test Result	Average strength	ITR Value	Variation
① For M30 38.0 34.2 29.0 35.1	34.07 > 34 N/mm <sup>2</sup> OK	Min strength 29 > (f <sub>ck</sub> - 3) 29.7    30.3 = 27 OK	38 - 34.07 = 3.93 3.93 → $\frac{3.93 \times 100}{34.07}$ = 11.54% 29 - 34.07 = -5.07 $\frac{-5.07 \times 100}{34.07} = -14.88\%$ OK
② for m30 42.0 38.0 36.4 34.1	37.624 N/mm <sup>2</sup> > 34 N/mm <sup>2</sup> OK	f <sub>ck</sub> - 3 = 27 34.1 > 27	$\frac{4.376 \times 100}{37.624} = 11.63\%$ $\frac{-3.524 \times 100}{37.624} = -9.3\%$ OK

#8 Acceptance Criteria for Design Mix:-  
(at the time of design mix)

→ At the time of design mix avg strength of 3 or 4 sample tested shall not be less than mean strength value ( $f_m$ ), called Target Mean strength of concrete:

$$f_m = f_{ck} + 1.65\sigma$$

#9 Young's Modulus of Elasticity of concrete :->

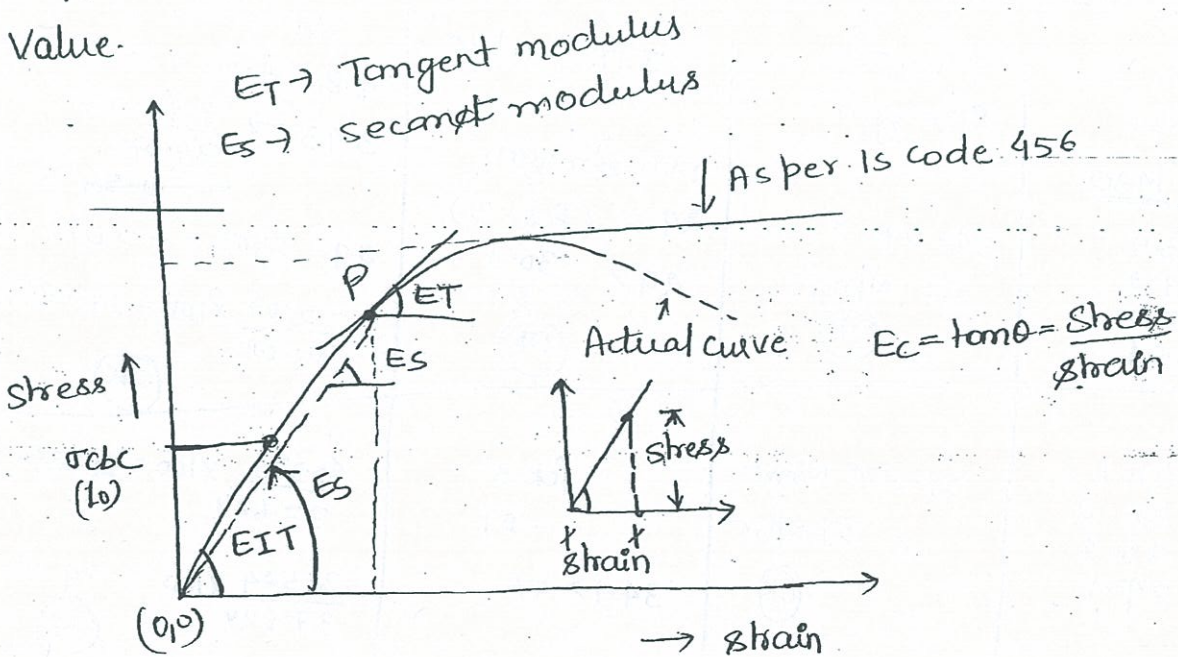
$$E_c = \frac{\text{Stress}}{\text{Strain}} = 5000 \sqrt{f_{ck}} \text{ (by IS code 456)}$$

\* The value suggested by code IS 456/2000

$E_c = 5000 \sqrt{f_{ck}}$  is short term static modulus of elasticity for concrete in  $N/mm^2$

Pr 6-2-3.1 / P-16

\* Actual value may differ by  $\pm 20\%$  from above value.



$$E_d = \frac{E_c}{(1+\theta)} = \frac{5000\sqrt{f_{ck}}}{(1+\theta)}$$

where,  $\theta \rightarrow$  creep coefficient

Age of concrete at the time of initial loading.	7 days (after 7 days loading)	28 days	1 year
Creep coeff ( $\theta$ )	2.2 ↓ 2.2 times the creep coeff.	1.6	1.1

$$E_c = \frac{\text{stress}}{\text{strain}} = \frac{P/A}{(\delta x/l)}$$

Total strain after very long time  
 $= (\delta x + \delta y)$

Creep strain =  $\theta \times$  Elastic strain  
 $\delta y = \theta \delta x$

$$\delta x + \delta y = \delta x + \theta \delta x$$

$$\Rightarrow E_d = \frac{\text{stress}}{\text{Total strain}} = \frac{P/A}{(1+\theta)(\delta x/l)} = \left(\frac{E_c}{1+\theta}\right) = \frac{5000\sqrt{f_{ck}}}{(1+\theta)}$$

whatever is the age of loading (e.g. for M30)

$$7 \text{ days} \Rightarrow E_d = \frac{5000\sqrt{f_{ck}}}{1+\theta}$$

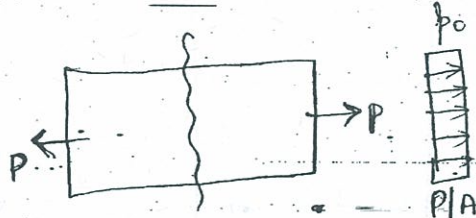
$$= \frac{5000\sqrt{30}}{1+2.2} = 2558.16 \text{ N/mm}^2$$

$$28 \text{ days} \Rightarrow E_d = \frac{5000\sqrt{30}}{1+1.6} = 10533.126 \text{ N/mm}^2$$

$E_c$  Value get reduced by 2 to 3 times due to Creep.

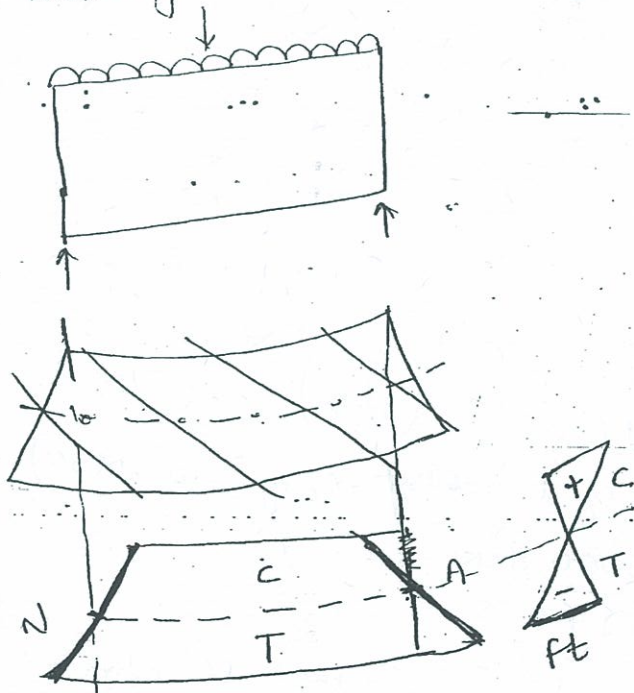
# 11 Tensile strength of concrete :-

① Direct tensile strength :-



Due to a direct tensile force  
 Direct strength =  $p_0 = P/A$   
 stress developed

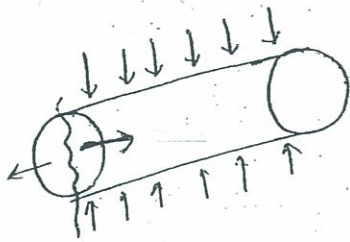
② Bending Tensile strength :-



⇒ In case of bending maxm permissible stress that can be taken by concrete is called - flexural tensile strength. also called modulus of rupture. ( $f_{cr}$ )  
 $f_{cr} = 0.7 \sqrt{f_{ck}}$   $f_{ck} \rightarrow$  char. strength



③ Split Tensile strength :



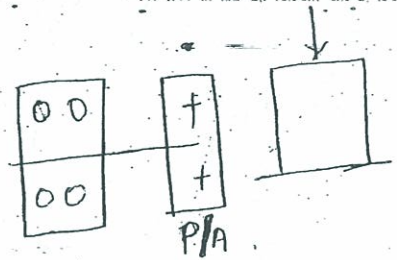
#12

MAX<sup>m</sup> Compressive strength

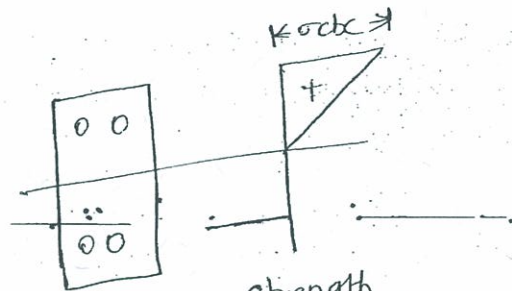
① In direct Compression ( $\sigma_{cc}$ )

$$\sigma_{cc} = P/A$$

= Max<sup>m</sup> permissible stress  $P_n$   
direct compression



② In bending compression  
( $\sigma_{cbc}$ ) due to bending



WSM

	Tensile strength Direct	flexural strength (Bending) ( $f_{cr}$ )	Compressive strength	
			Direct ( $\sigma_{cc}$ )	Bending ( $\sigma_{cbc}$ )
M15	2	2.71	4.0	5.0 } 2
M20	2.8	3.13	5.0	7.0 } 1.5
M25	3.2	3.50	6.0	8.5 } 1.5
M30	3.6	3.83	8.0	10.0 } 1.5
M35	4.0	4.14	9.0	11.5 } 1.5
M40	4.4	4.43	10.0	13 } 1.5
	N/mm <sup>2</sup>	N/mm <sup>2</sup>		N/mm <sup>2</sup>

⑤ Steel Reinforcement :-

Types :-

① Mild steel (Fe 250)

$f_y = 250 \text{ N/mm}^2 = \text{characteristic strength}$   
 yield or stress

→ strength in tension (WSM)  
 $\sigma_{st} = 140 \text{ N/mm}^2$  (upto 20mm  $\phi$  bars)

→ Low strength

→ High ductility

→ (Very good in earthquake) → deform takes time

② Medium tensile steel

$\sigma_{st} = 190 \text{ N/mm}^2$

→ medium strength

③ Cold twisted bars CCTD  
 or  
 HYSD (High Yield Deformed Bars)

Fe 415 or Fe 500 or higher

→ high strength

→ Low ductility

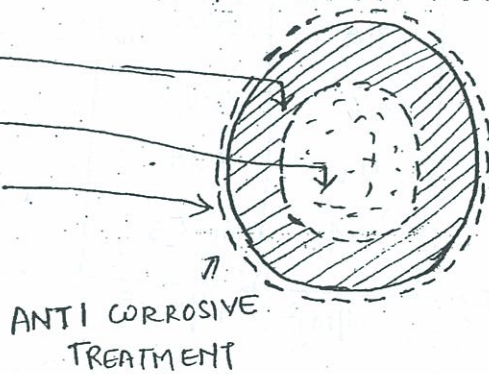
④ TMT Bars (Thermo Mechanically Treated bars)

\* Fe 415 / Fe 500 / Fe 550 / Fe 600 / or higher

→ High strength

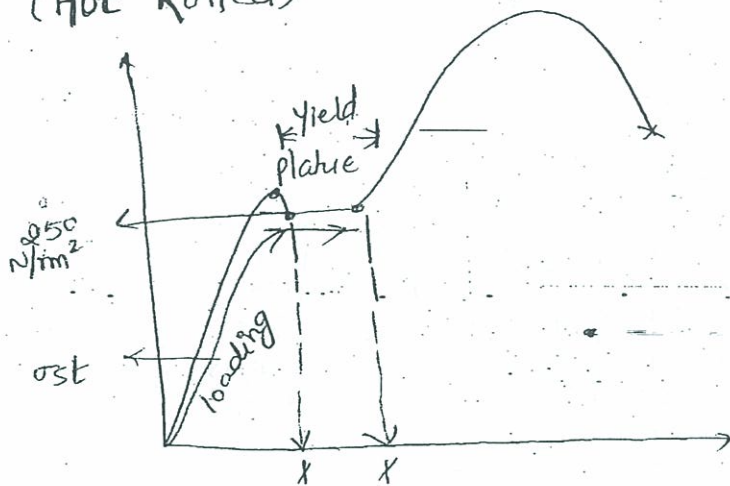
→ High ductility

→ Corrosion resistant



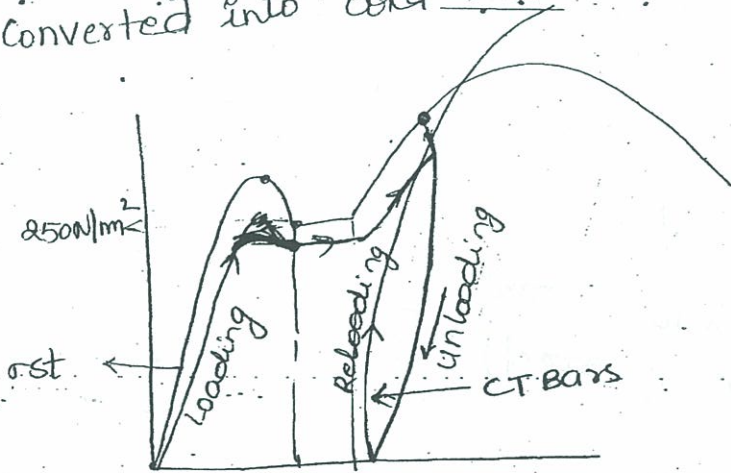
(#) Stress-strain curve :-

(L) Mild steel (Hot Rolled)



→ Mild steel reinforcement undergoes large amount of deformation at yield plateau.

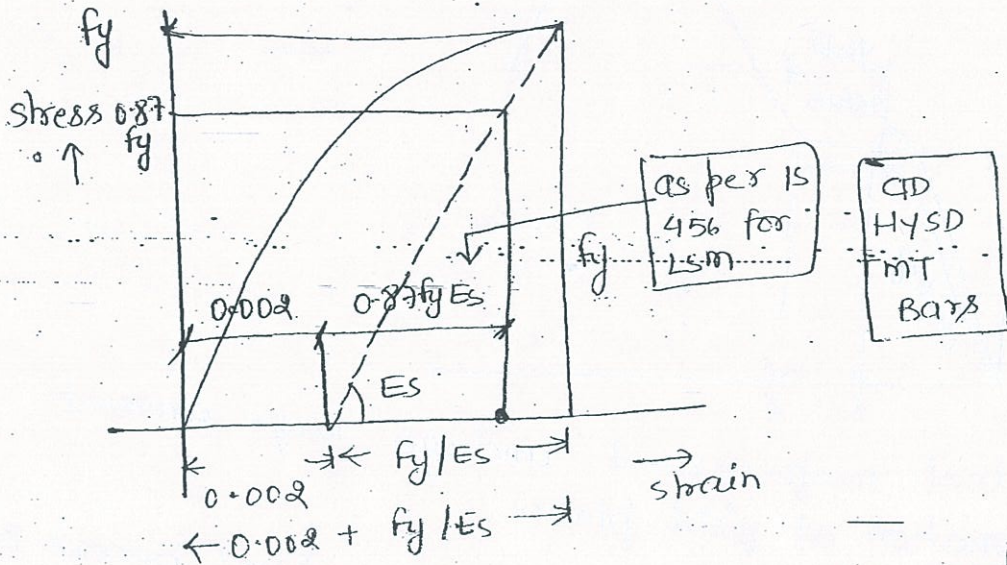
→ To avoid yield plateau "cold working" process is used for mild steel. By cold working mild steel is converted into cold twisted bars.



Cold working process

\* Cold working: In cold working the steel reinforcement is stretched beyond yield plateau either by stretching or by twisting and then by unloading it.

⊕ A cold twisted bar does not show a well defined yield point.



\* For such steel yield stress value is read at 0.002 strain (0.2% strain) (Proof strain value) by drawing a parallel to stress-strain curve line

Total strain at yield stress value

$$= 0.002 + \frac{f_y}{E_s}$$

\* Value of  $E_s = 2 \times 10^5 \text{ N/mm}^2$  (for all type of steel)

① For Fe 415

Total strain at yield limit

$$= \left( 0.002 + \frac{415}{2 \times 10^5} \right) = \boxed{0.004075}$$

② For Fe 500

$$= 0.002 + \frac{500}{2 \times 10^5} = \boxed{0.0045}$$